18 July 1967

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Corning Glass Works 3900 Electronics Drive Raleigh, North Carolina

Deer Mort:

Pursuant to our telephone conversations on 10 and 13 July, I'm sending you the information you requested about the Image Intensifier Screen and also the information I volunteered about the screen material used on the Czechoslovakian Mosaic Screen at EXPO 67.

The information on the Image Intensifier Screen is attached in the form of our old Development Objectives. It's my understanding that you have something you think may be applicable -- I want to reemphasize the point that we've had to set this development aside pending advances in the state-of-the-art, a higher priority requirement and/or more R&D funds. However, we're always interested in learning of new technology; so if you believe that you have something of interest to share, you know we would appreciate it.

On the second matter, I'll verify the information I gave you over the phone as follows:

1. The rear projection screen material used on the Czech Mosaic Screen System at EXPO 67 appeared to have much higher contrast than any other I have seen.

2. Tasked about the material and was directed to see He informed me that the material did
have very high contrast and that he had discovered it in West Germany.
It was developed in a small company under the direction of a
However, he purchased the material from:

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	Sincerely yours,	
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13 July 1967 (Retype of Document originally dated 2 November 1964)

DEVELOPMENT OBJECTIVES

IMAGE-INTENSIFIER SCREEN

1. INTRODUCTION

These development objectives describe requirements for an imageintensifier screen to be used for rear-projected images.

Rear-projection viewers have come into standard use for scanning and interpreting photo transparencies. Most of these materials are high resolution and require great enlargement before the human visual system can assess the total information content. This enlargement, in turn, requires greater projection lamp power in order to attain the necessary image brightness over the entire viewing screen. Increased lamp power is accompanied by greatly increased heat incident on the film so that it is distorted or damaged. There are in existence various techniques for cooling at the film plane, e.g.. dichroic mirrors, fans, liquid gates, etc. In spite of these techniques, there remains the heat vs image intensity problem in high magnification projection of film transparencies which are static or slow moving in the film gate.

It has been postulated that this problem might be solved by intensifying the image at the viewing screen. Such a screen would require minimal power in the projection illumination, but would produce a bright image for the viewer.

2. CONCEPT

- 2.1 <u>Purpose</u>. These objectives describe a development which would overcome the heat versus image intensity relationship characteristic of high magnification (in the order of 100X) rear projection viewers.
- 2.2 Scope. The primary objective is, that under nominal highlight illumination of approximately 10 foot candles, the image-intensifier screen should provide the viewer with an image of adequate gain and brightness while exhibiting satisfactory performance in many other aspects, such as: resolution, tone range, linearity, color temperature, viewing angle, response time, size, life and cost.

A secondary objective is to provide a means for controlling modulation of image contrast, such as tone-reversal and compression or expansion.

3. GENERAL DESCRIPTION

The image-intensifier screen is intended for use on rear-projection viewers, which would be used by one to four persons to scan and interpret high-quality photo transparencies at various magnifications (ranging to 100X). The screen size on these viewers may be as large as 30" x 30". The image-intensifier screen should be designed to require minimum modification of existing viewers.

4. PRIMARY REQUIREMENTS

4.1 Gain. The gain of the IIS must be such that light within the range of 2800°- 5800°K, falling on the screen at intensity equal to one foot-candle, causes a brightness of 50 foot-lamberts to be radiated throughout a solid angle of 90° (centered on the axial ray). A greater gain is desired--provided that it does not compromise other performance parameters.

4.2 Emitted Light.

- 4.2.1 <u>Brightness</u>. The IIS must be capable of emitting a maximum brightness of 50 foot-lamberts; 200 foot-lamberts is the development goal.
- 4.2.2 <u>Linearity</u>. Gamma. The emitted light must be directly proportional to the incident light at all intensities. Gamma must approximate unity (+ 10%).
- 4.2.3 Brightness should not vary more than 10% (from the theoretical) over the entire viewing area.
- 4.2.4 <u>Brightness Distribution Lobe</u>. The emitted light should be of relatively uniform brightness (+ 10%) throughout a 90° solid angle centered on the emergent axial ray.
- 4.2.5 Color Temperature. The emitted light must fall within the color temperature range of 3500 5500 K.
- 4.2.6 <u>Brightness Levels</u>. The emitted light must display at least ten different, visually distinguishable brightness levels when excited by correspondingly varied incident illumination. As many as twenty different distinguishable levels are desired.
- 4.2.7 Reflectance. The viewing surface of the IIS shall be designed to minimize reflectance of ambient room light. This requirement is of utmost importance: ideally the viewing surface of the IIS should have reflectance characteristics similar to those of black velvet, in order that maximum modulation transfer can be preserved even in normal room light.

- 4.3 Resolution. The IIS shall be capable of resolving 10 line pairs per millimeter with a contrast of 100 to 1. The modulation transfer function at 10 lines/mm should be at least 90%: 20 lines/mm at 90% MTF is the design goal.
- 4.4 Response Time. The IIS must reach 90% theoretical brightness within 10 milliseconds of excitation and must fall below 10% of this brightness level within 10 milliseconds of removal.
- 4.5 <u>Signal/Noise Ratio</u>. No square inch of the IIS should exhibit a signal/noise ratio less than 100.
- 4.6 <u>Size</u>. The thickness-and weight-to-area ratio of the IIS should be approximately that of a conventional screen. This IIS may be breadboarded in 6" x 6" panels. One 12" x 12" operational panel must be delivered. Optional pricing for delivery of a 30" x 30" panel may be given. Feasibility of producing the 30" x 30" units in volume must be indicated.
- 4.7 <u>Life Expectancy</u>. The IIS must be capable of operating at maximum brightness (at least 50 foot-lamberts) for 200 hours, with no more than 10% degradation in any of the specified performance parameters.
- 4.8 Power Requirements. The IIS should be adequately served by 110-120 volt, 60 cycle, 15 ampere power supply. Normal fluctuations in the voltage (+ 10%) should not perceivably affect performance.

5. SECONDARY REQUIREMENTS

The following requirements are to be considered if they do not compromise those stated in section 4 (above):

- 5.1 <u>Contrast Modulation</u>. If the capability is inherent, controllable contrast modulation of the following types is desired:
 - 5.1.1 Complete linear intensity reversal should be available at the option of the operator.
 - 5.1.2 Expansion and compression of the brightness range should be an option available to the operator.
- 5.2 Monochromatic Sensitivity. The IIS should be sensitive enough to accept illumination from a narrow band of the visible spectrum or the near IR and UV: 6328 AO laser illumination would be a logical consideration. If such were feasible, lens design could be optimized accordingly. In such a case the gain requirements described in 4.1 would be modified correspondingly.